

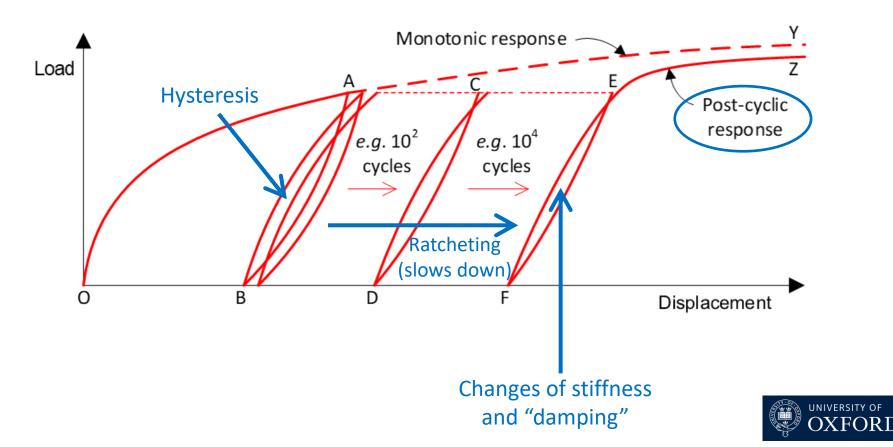
Theoretical modelling of cycling using HARM

Dansk Geoteknisk Forening, 24th September 2024

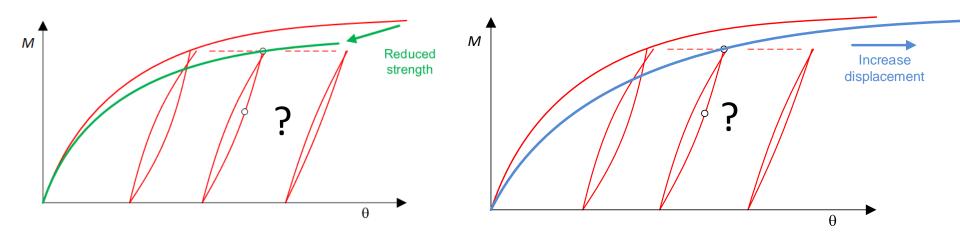
Prof. Guy Houlsby

Professor Emeritus, Department of Engineering Science, Oxford University

Phenomena to be modelled during cycling



Typical "scaling" design methods for cycling (unsatisfactory)

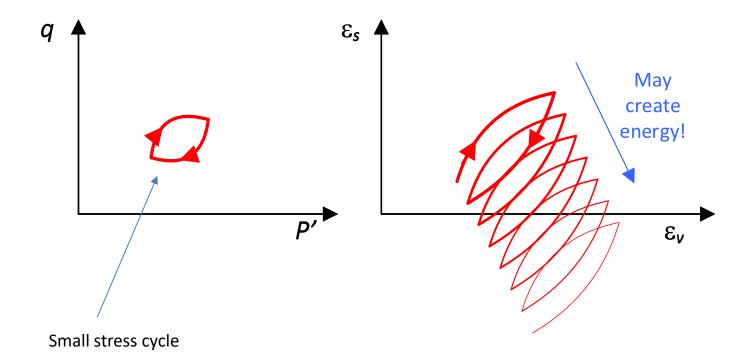


Reduced strength at constant stiffness

Increased displacement at constant strength

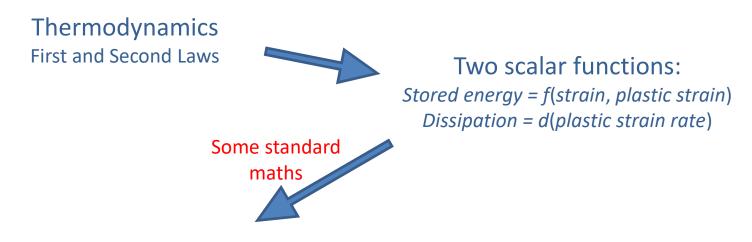


Why is thermodynamics important in cycling?





Hyperplasticity



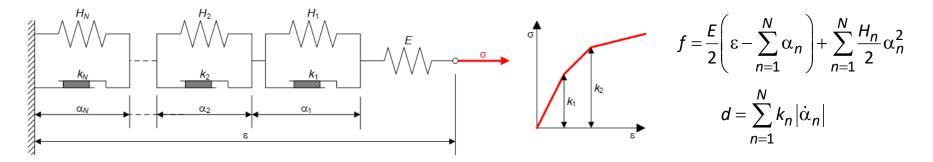
Plasticity model: Stored energy = f(strain, plastic strain) Yield surface = y(stress, etc)



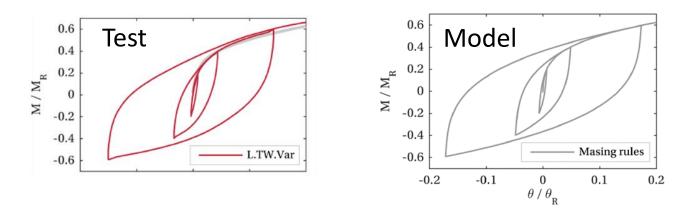
Model non-linearity in cyclic loading



Modelling cycling with "multisurface plasticity"



.... automatically obeys "Masing rules" on cycling

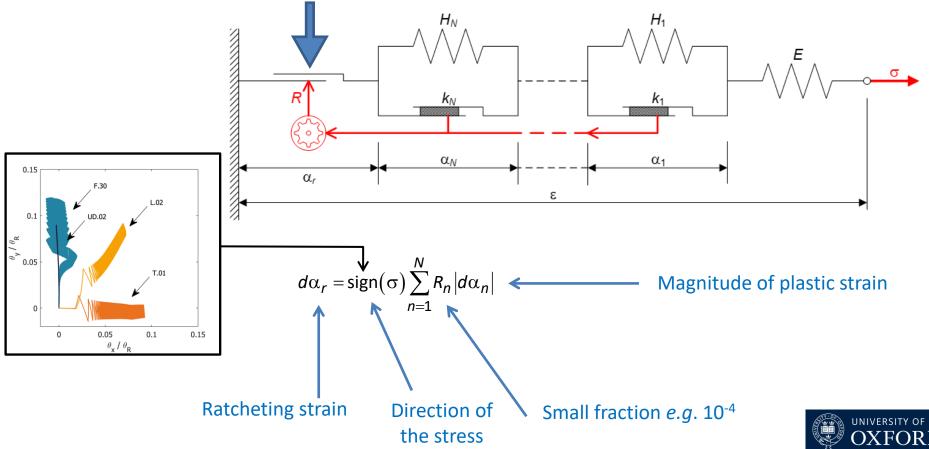




Figures from Richards (2019)

Modelling ratcheting: the "HARM" approach

Add a special "ratcheting element", giving a small additional displacement

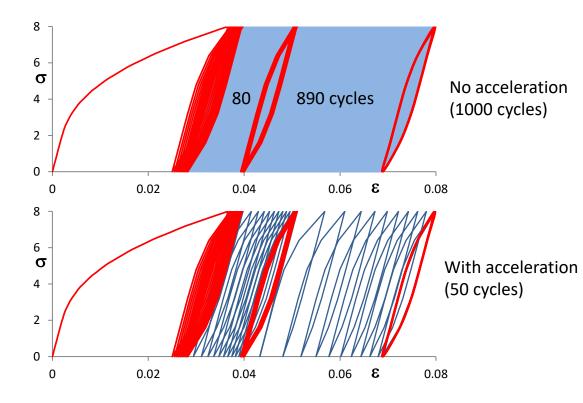


Scaling of ratcheting ("Acceleration")

$$d\alpha_r = \frac{R_{fac}}{R_{fac}} \operatorname{sign}(\sigma) \sum_{n=1}^{N} R_n |d\alpha_n|$$

Complete model definition

$$f = \frac{E}{2} \left(\varepsilon - \sum_{n=1}^{N} \alpha_n - \alpha_r \right)^2 + \sum_{n=1}^{N} \frac{H_n}{2} \alpha_n^2$$
$$d = \sum_{n=1}^{N} k_n |\dot{\alpha}_n| + (\sigma \dot{\alpha}_r)$$
$$+ \Lambda_r \left(\dot{\alpha}_r - \frac{R_{fac}}{S} S(\sigma) \sum_{n=1}^{N} \frac{R_n |\dot{\alpha}_n|}{n} \right)$$
$$+ \Lambda_h (\dot{\beta} - |\dot{\alpha}_r|)$$
$$R_n = f(\beta)$$



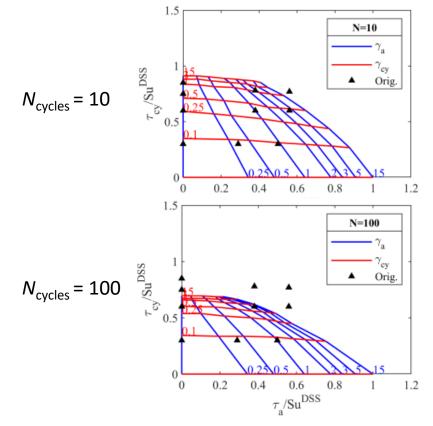


Continuum models (1): Clay

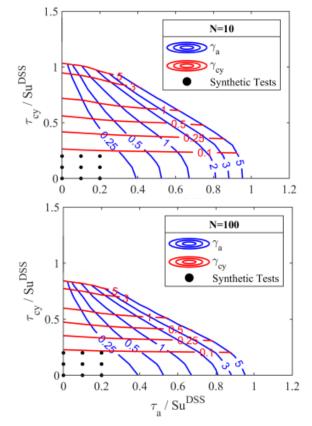
- Develop a model for undrained clay in Direct Simple Shear
 - Includes <u>rate effects</u> and <u>ratcheting</u>
- Use model to compare with NGI "contour diagram" approach for predicting strains during cycling
 - Create artificial contour diagrams from the model to compare with NGI



Compare with NGI contour diagrams



NGI tests on Drammen Clay: empirical contour diagram



Synthetic contour diagram generated by HARM model

Modelling by Toby Balaam

Continuum models (2): Sand

- Develop "HySand" model for sand in triaxial tests
- Compare with Torsten Wichtmann's database of cyclic tests
- Generalised to general stress states
- Impemented in FE codes ABAQUS and PLAXIS



HySand – a constitutive model for sand under cyclic loading

Hyperplasticity: entire model defined by two functions:

$$g = -\frac{p_r}{k_r(1-m)(2-m)} \left(\frac{p_0}{p_r}\right)^{2-m} - \frac{1}{N} \sum_{n=1}^N \sigma : \alpha^{(n)} - \frac{1}{N} \sum_{n=1}^N \frac{l_{1\sigma}}{3} \alpha_{pc}^{(n)}$$

$$y^{(n)} = \frac{4I_{1\sigma}J_{2X^{(n)}} - 3\mathrm{tr}\left(\sigma X^{(n)^2}\right)}{8\left(\frac{n}{N}\mu\right)^2 I_{3\sigma}} + \left(\frac{N\chi_{pc}^{(n)}}{p_c^{(n)}}\right)^r - 1 = 0$$

$$\mathbf{X}^{(n)} = \cdots, \quad p_0 = \cdots, \quad \beta = \cdots, \quad \text{etc.}$$

ſ	k _r	g_r	т	$arphi_c$	β_{max}	В	Г	Δ	λ_{Γ}	λ_Δ	A _{max}	h_0	b	r
	516	400	0.7	33.1	1.0	2.057	1.98	1.677	0.0032	0.0008	40	750	3	0.3



Work by Luc Simonin

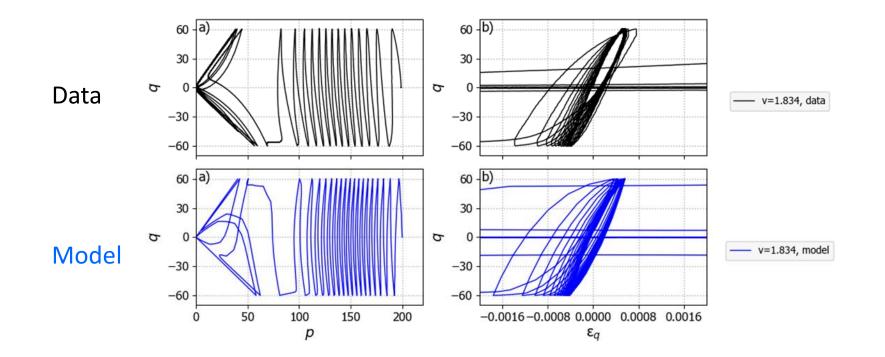
Monotonic tests

800 b) 0.02 a) 0.00 600 v0=1.975, data Drained -0.02 v0=1.824, data β or 400 tests at v0=1.748, data -0.04v0=1.975, model different 200 v0=1.824, model -0.06 densities v0=1.748, model -0.08 -0 0.04 0.08 0.12 0.16 0.20 0.00 0.04 0.08 0.12 0.16 0.20 0.00 εq εq 500 500 b) a) 400 400 Undrained v=1.946, data tests at 300 300 v=1.814, data g β different v=1.728, data 200 200 v=1.946, model densities v=1.814, model 100 100 v=1.728, model 0 0 160 80 240 320 400 0.00 0.01 0.02 0.03 0.04 0.05 0 р εq



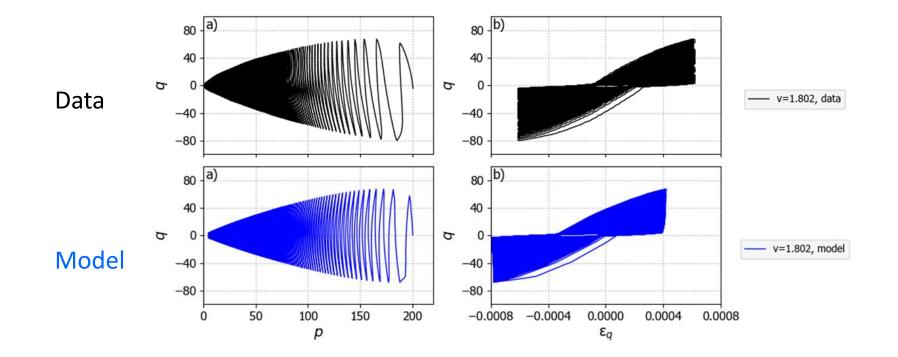
Data by Wichmann, modelling by Simonin

Cyclic tests: stress controlled



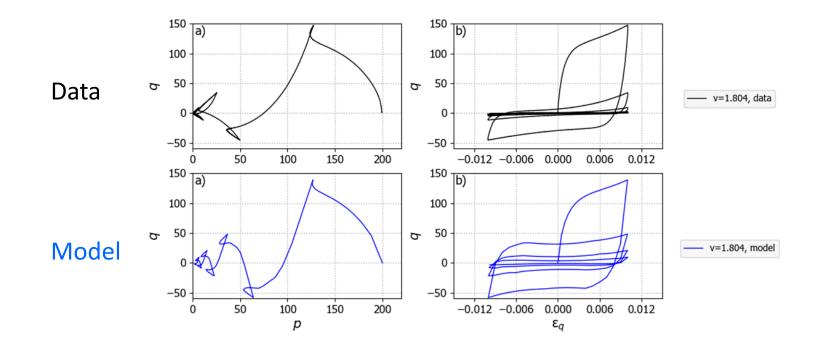


Cyclic tests: strain controlled (small cycles)





Cyclic tests: strain controlled (large cycles)





... final remarks

- Modelling cyclic loading
- Hyperplasticity ensures that the models obey thermodynamic principles
- HARM is a method to add ratcheting to basic multisurface models
 - Reproduces "contour diagrams"
- HySand models cycling of sand
 - Reproduces Wichtmann's data well



